Assignment 2

Due date: 8th October 2013

Value: 20%

Marking scheme

The distribution of marks is given in the table below.

The student should provide some explanation of how he/she arrives at an answer. This explanation can be in the form of an equation that the student states or it could be in the form of a brief description of his/her reasoning.

The student will score full marks (as per the table below) if he/she gives the right answer together with a correct explanation (or equation).

For each part, the student can lose up to 35% of the marks if the answer is right, but no explanation is given or the explanation is inadequate.

For each part, the student will be able to score up to 80% of the marks if the answer is wrong but the explanation is correct or partly correct.

Question	(a)	(b)	(c)	(d)	(e)	Total
1	5	5	5	5		20
2	4	4	4	4	4	20
3	4	4	4	4	4	20
4	5	5	5	5		20
5	5	5	5	5		20
6	5	5	5	5		20
7	10	10				20
8	5	5	5	5		20
9	4	4	4	4	4	20
10	4	4	4	4	4	20
Total marks						200

This question relates mainly to **Module 7** phase-controlled thyristor converters and the third objective in the course specification.

Use the waveform template given in your introductory book.

Refer to **figure 7.10** of your study book.

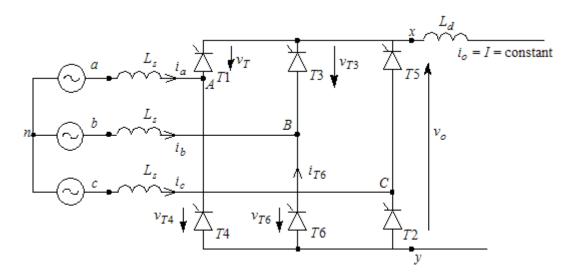


Figure 7.10: Three-phase thyristor converter $(L_s - \text{supply inductance})$

Assume all components are ideal.

 v_{an} (in volts) = 155.6 sin ωt ω = 120 π rad/s I = 20 A α = delay angle = 75°

For $L_s = 0$ mH

- (a) Calculate the mean value of v_o
- (b) Sketch waveform for v_o , v_{T3} and i_{T5}

For $L_s = 0.5 \text{mH}$

- (c) Calculate the mean value of v_o
- (d) Sketch waveform for v_o , v_{T3} and i_{T5}

This question relates mainly to **Module 7** phase-controlled thyristor converters and the third objective in the course specification.

Refer to **figure 7.24** of your study book.

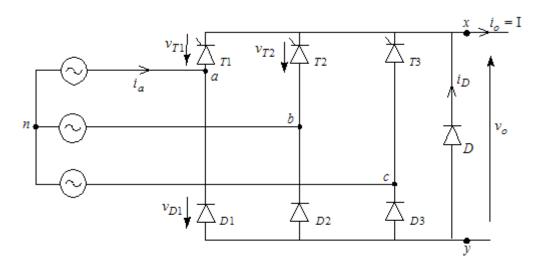


Figure 7.24: Three-phase half controlled rectifier

Assume all components are ideal.

 v_{an} (Volts) = 311 sin ωt ω = 100 π rad/s I = 20 A α = delay angle

For delay angle $\alpha = 30^{\circ}$ sketch waveforms for:

- (a) v_o and v_{Tl}
- (b) i_a and i_D

For delay angle $\alpha = 105^{\circ}$ sketch waveforms for:

- (c) v_o and v_{Tl}
- (d) i_b and i_D
- (e) Calculate the rms value of i_D for delay angle $\alpha = 105^{\circ}$.

This question relates mainly to **Module 8** switch-mode inverters and the third objective in the course specification.

Refer to the circuit in **figure 8.12** of the study book.

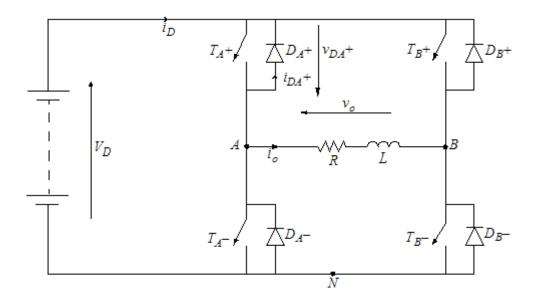


Figure 8.2: Single-phase square wave bridge inverter – R-L load

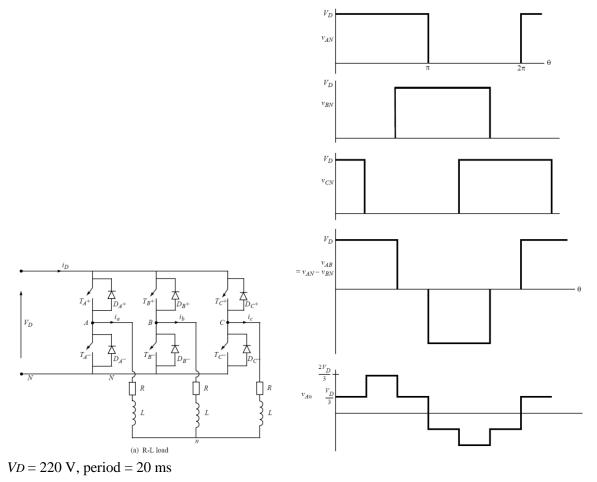
Assume all components are ideal and v_o is a square wave (unmodified).

 $V_D = 400 \text{ V}; \quad R = 10 \Omega; \quad L/R = 25 \text{ ms}; \quad T = 10 \text{ ms}$

- (a) Calculate \hat{I}_{φ}
- (b) Sketch waveforms for the current through the diode D_B +
- (c) Sketch waveforms for the voltage across the diode D_B +
- (d) For what fraction of the period does D_B + conduct?
- (e) Calculate the rms value of the fundamental component of i_o .

This question relates mainly to **Module 8** switch-mode inverters and the third objective in the course specification.

Refer to the circuit in **figure 8.12(a)** of the study book. The voltage waveforms in **figure 8.13** are applicable. Circuit operation is at steady state. The mean values of *ia*, *ib* and *ic* are all equal to zero.

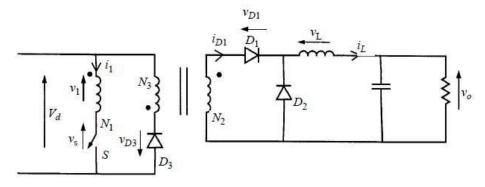


For R = 0, L = 0.1 H,

- (a) Sketch waveforms for v_{Cn} and \dot{i}_c .
- (b) Calculate the peak value of i_c and the rms value of the fundamental component of i_c

For
$$R = 20\Omega$$
, $L = 0$ H,

- (c) Sketch waveforms for v_{Cn} and \dot{i}_c
- (d) Calculate the peak value of i_c and the rms value of the fundamental component of i_c





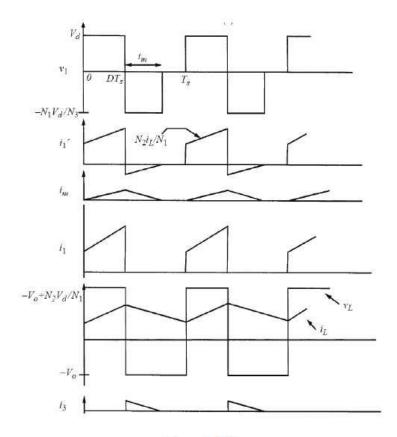


Figure 9.7 (b)

 $V_d = 230$ V; $V_o = 80$ V; $1/T_s = 15$ kHz; $N_3 = N_1$; $L = 200\mu$ H; C = 18 μ F.

(a) Calculate the minimum allowable value of N_2/N_1

(b) Estimate the peak to peak ripple in *vo*. Assume $N_1 = N_2$

(c) Sketch waveforms for v_{D3}

(d) Sketch waveforms for i_{D3} .

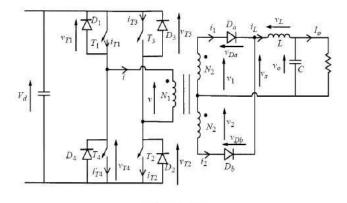


Figure 9.13

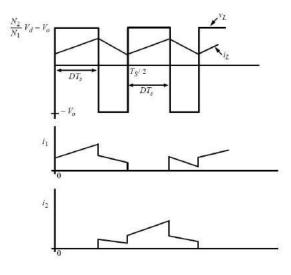


Figure 9.13c

 $V_d = 300$ V; $I_0 = 5$ A; $V_0 = 48$ V; $1/T_s = 20$ kHz; $N_2/N_1 = 0.25$

(a) Calculate the value of *D*.

(b) Calculate the minimum value of *L*, if the peak to peak ripple content in i_L is to be maintained below 15% of I_L .

(c) Sketch waveforms for v_{T2} .

(d) Sketch waveforms for i_{T2} . Indicate the peak value of i_{T2} .

You may assume equal sharing of voltages by the transistors when all of them are off. Assume L = 1.5mH.

Part (a)

This question relates mainly to **Module 10** drives overview and the fourth objective in the course specification.

A motor is operated at full load and at rated speed for **6 minutes** and then it is operated at no-load for **12 minutes**.

This operating cycle is continuously repeated resulting in motor insulation temperature changing periodically.

As a first approximation the thermal behaviour of the insulation can be modelled as that of a first order system with a thermal time constant τ of **30 minutes** and a thermal resistance of **0.2° C/W**.

Motor power losses at full load = 550 W

Motor power losses at no-load = 220 W

Insulation temperature rise above ambient while the motor is loaded is given by:

$$T=T_1 T_2 e^{-t/\tau}$$

where t = 0 at the instant load is applied to the motor.

*T*¹ is the insulation temperature rise above ambient that would be reached if the motor was to be left fully loaded for a very long time (i.e. *t* approaches infinity).

Insulation temperature rise above ambient while the motor is running idle is given by:

$$T=T_3 T_4 e^{-t/\tau}$$

where at the instant load is removed from the motor.

*T*³ is the insulation temperature rise above ambient that would be reached if the motor was to be left energised but unloaded for a very long time (i.e. approaches infinity).

Calculate the values of *T*1, *T*2, *T*3, *T*4. Deduce the peak value of the insulation temperature. Sketch motor insulation temperature rise against time.

Part (b)

This question relates mainly to **Module 10** drives overview and the fourth objective in the course specification.

One cycle of the motion profile of a purely inertial load is described below:

Time	Description of motion	
0 – 5 s	constant acceleration from 0 rad/s to 300 rad/s	
5 s – 10 s	constant speed at 300 rad/s	
10 s –15 s	constant deceleration from 300 rad/s to 150 rad/s	
15 s – 25 s	constant deceleration from 150 rad/s to 0 rad/s	
25 s – 30 s	stationary	

Combined moment of inertia = 12 kgm^2 .

Neglecting all losses; The load is directly coupled to the motor.

(a) Calculate the peak torque required from the motor.

(b) Calculate the rms value of the motor torque.

This question relates mainly to **Module 11**. DC adjustable speed drives and the fifth objective in the course specification.

Refer to the circuit in **figure 11.6** of the study book.

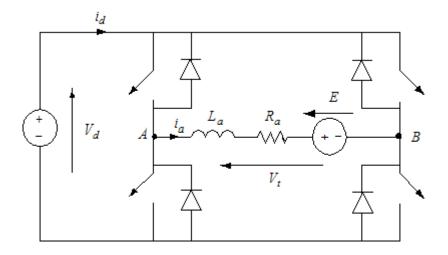


Figure 11.6: Four quadrant DC drive (ϕ_f constant)

Assume all components in the converter are ideal.

 $V_d = 200 \text{ V}; \quad K_E = 0.6 \text{ V/(rad/s)}; \quad L_a = 15 \text{ mH}; \quad R_a = 0.5 \Omega$

The unipolar control method is used to operate the bridge. Transistor switching frequency is 1.5 kHz.

If speed is 1500 r/min and I_a is 0A draw waveforms for:

(a) v_t and

(b) i_a .

If speed is 1500 r/min, but in reverse direction compared to the above, and I_a is 20 A.

The motor is in regenerative braking mode, draw waveforms for:

- (c) v_t and
- (d) i_a . Indicate maximum and minimum values of i_a .

This question relates mainly to **Module 11**. DC adjustable speed drives and the fifth objective in the course specification.

Consider the circuit in **figure 11.14(a)** of the study book.

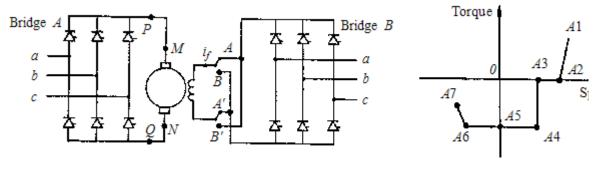


Figure 11.14(a)

Figure 11.14(b)

The line to line voltage of the three phase AC supply is **415** V. While motoring at point **A1**, **figure 11.14(b)**, the load torque, including friction torque is equal to **50** Nm and the speed is equal to **1000** r/min. Current limit, positive or negative, is set at **50** A. Values for some of the motor parameters are given below:

$$K_E = 1.2 \text{ V/(rad/s)};$$
 $K_T = 1.8 \text{Nm/A};$ $R_a = 0.75 \Omega$

The values of K_E and K_T correspond to rated field current.

While motoring at **point A7**, **figure 11.14(b)**, the load torque is 20 Nm and the speed is **1250 r/min**. Compared to operation at **point A1**, field current has reversed, but its magnitude is unchanged. The magnitude of the field current is equal to its rated value at all times, except during reversal between **point A2** and **point A3** in **figure 11.14(b)**.

Neglect the effect of supply inductance. Assume that there is no speed drop or rise from points A1 to A2, A3 to A4 and A6 to A7. There is a ten per cent speed drop from A2 to A3.

Determine the delay angles of **bridge A** during operation at points:

(a) A1

- (b) A4
- (c) A5
- (d) A6 and

(e) A7.

This question relates mainly to the sixth objective in the course specification.

A 22kW, 440V, 50Hz, 4-pole cage induction motor is part of an adjustable speed drive system. At the base voltage and frequency, the full-load slip is 0.05. It can be assumed that the torque-speed characteristic of the motor is linear in the slip frequency range from -5 Hz to 5 Hz.

Combined moment of inertia of motor and $load = 12 kgm^2$.

Load torque in Nm = 5ω where ω is in rad/s.

The steady state operating speed ranges from 900r/min to 1400r/min.

Acceleration is required to be constant at 30rad/s^2 and deceleration is required to be constant at 60 rad/s².

The drive consists of a voltage source inverter with a three-phase diode rectifier at the front end. The supply voltage may be assumed to be 440V.

Estimate:

- (a) steady state-slip when speed is 1400r/min.
- (b) steady state slip when speed is 900r/min.
- (c) required electromagnetic torque during acceleration and during deceleration.
- (d) maximum DC input current to the inverter during acceleration (assume efficiency of motor-inverter combination is 91%).
- (e) acceleration time from zero speed to 1400r/min.